



# Hydraulic Modeling for the Three Rivers HC145 Structure

McClellan-Kerr Arkansas River Navigation System  
Arkansas and Desha Counties, Arkansas

Client: USACE, Little Rock District

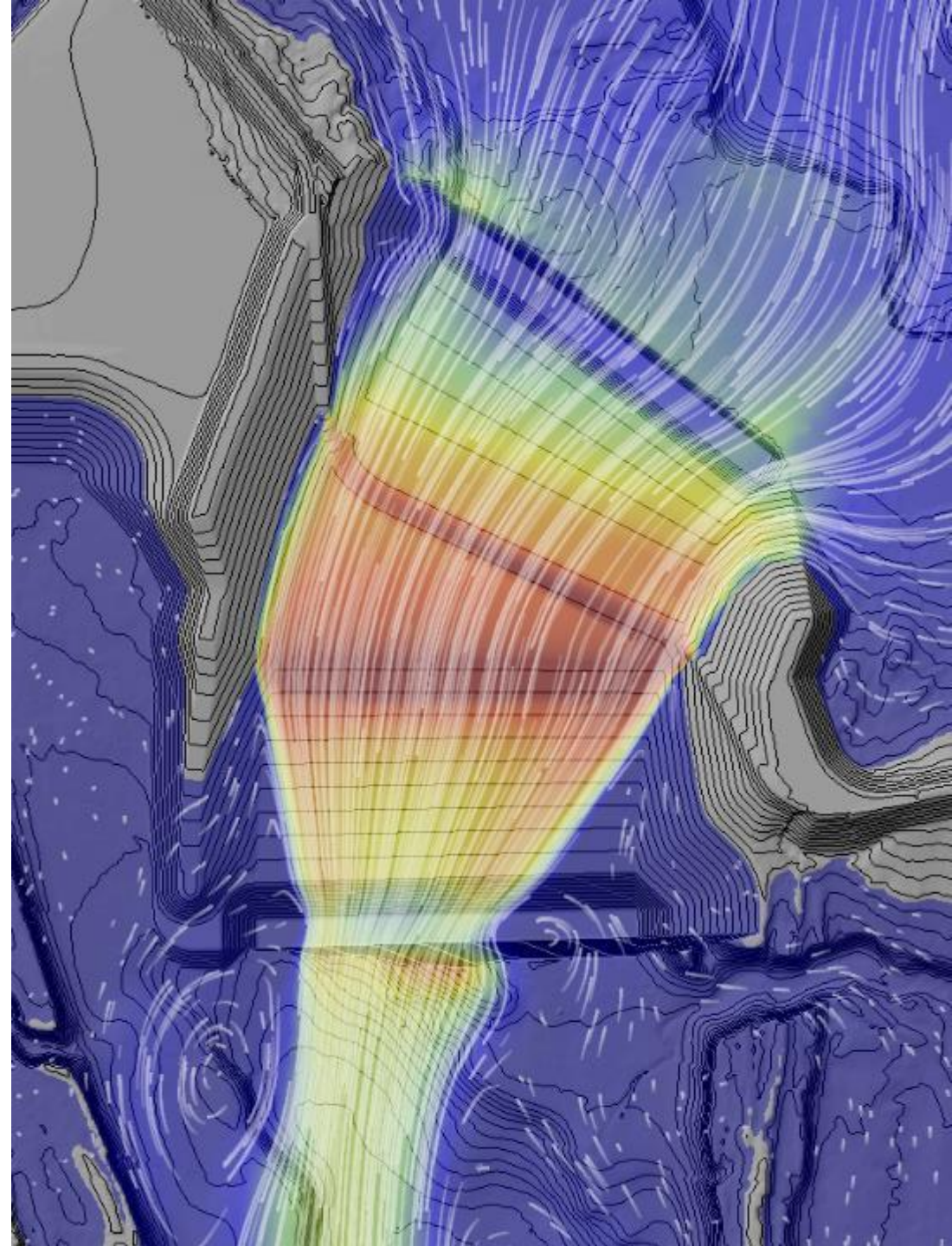


**2024 IAFSM Annual Conference**  
**March 12, 2024**

**Presentation by: Stantec Consulting Services Inc.**

Matthew Hoy, PE

Justin Bartels, PE, CFM





# Agenda

- **Project Background**
  - Project Location
  - Existing Conditions
  - Design Features
- **Hydraulic Analyses**
  - Hydraulic Modeling Framework
  - Design Criteria
  - 2D HEC-RAS Modeling
  - CFD Modeling (FLOW-3D HYDRO)
  - 1:20 Scale Physical Model Testing (Alden)
  - Sediment Transport Modeling (2D HEC-RAS)

Three Rivers, Phase 1 DB HC145

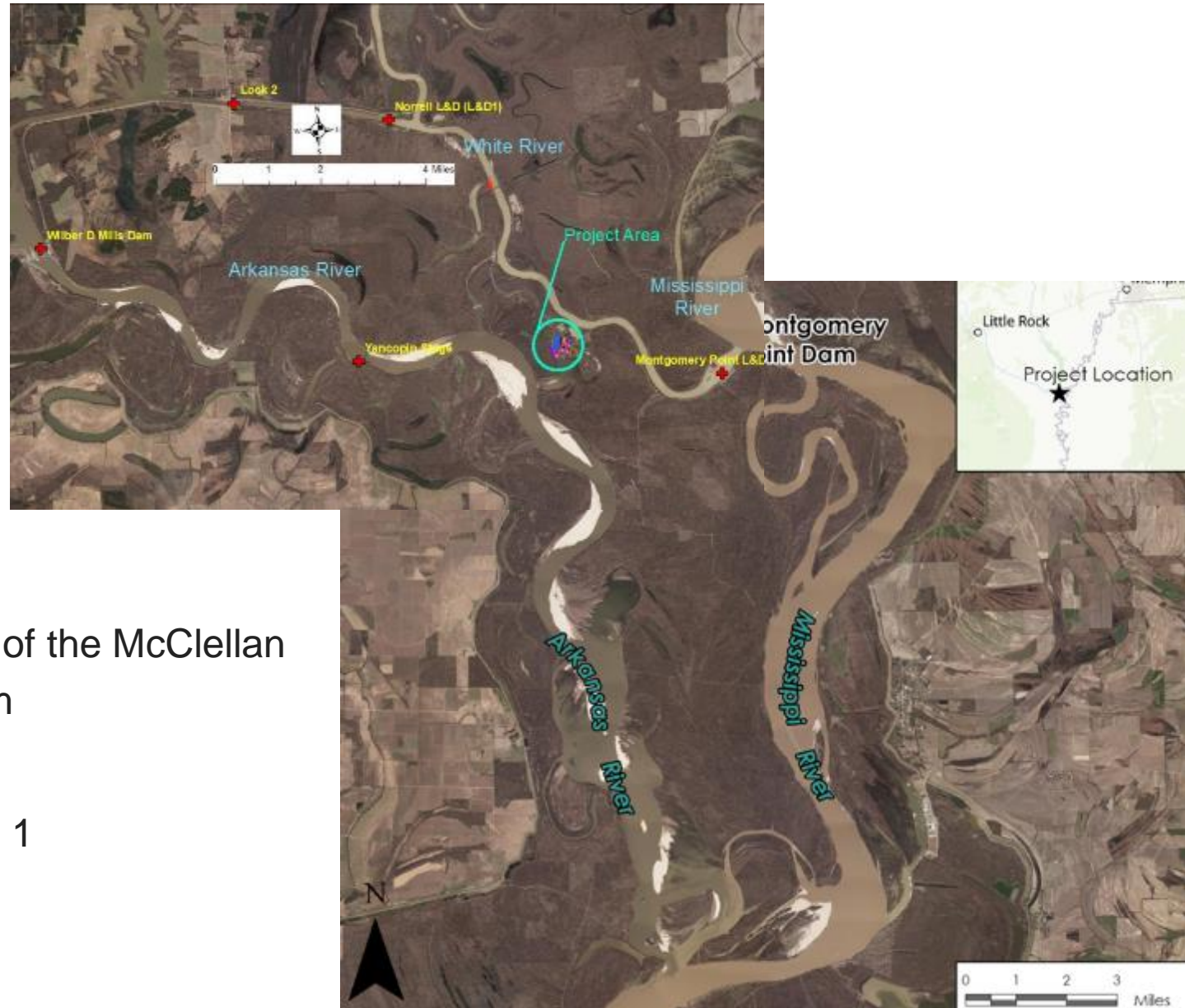
# Project Background





# Project Location

- The proposed weir structure will regulate flow between the White River and Arkansas River during high flow events
- Project area is located between three rivers:
  - Arkansas River
  - White River
  - Mississippi River
- Project is located at the southeast end of the McClellan Kerr Arkansas River Navigation System
- Two Phases – HC145 Project is Phase 1







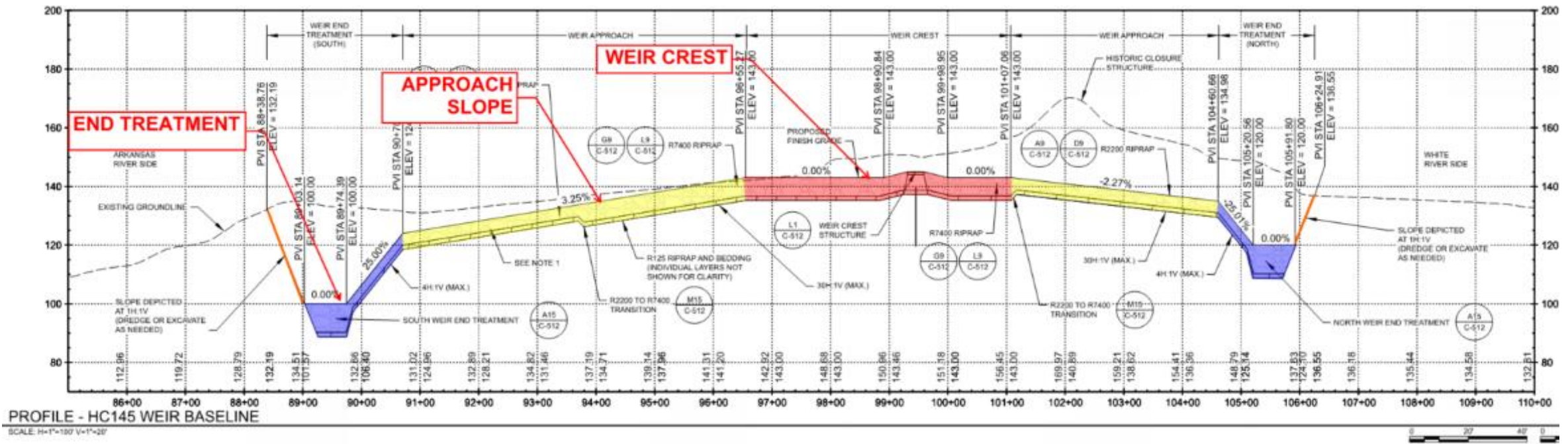
# Existing Conditions – Historic Closure







# Design Features



Three Rivers – HC-145 Project

# Hydraulic Analyses

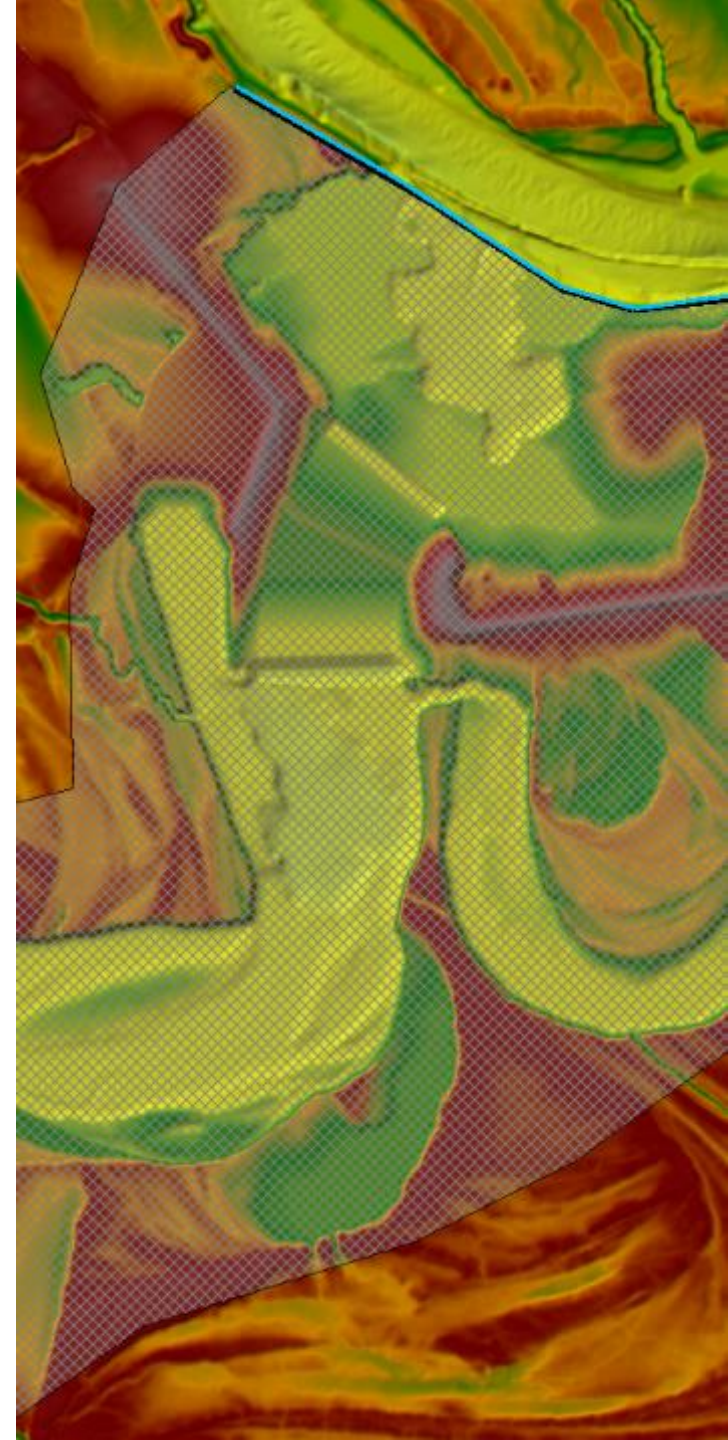




# Hydraulic Modeling Framework

Utilized a multi-component modeling approach, including:

- **2D Steady and Unsteady Flow Modeling (2D HEC-RAS)**
  - Large domain model to confirm boundary conditions at project
  - Small domain model for evaluating hydraulics through project
  - Estimate velocities and depths during design events to support riprap extents and sizing
- **CFD Modeling (FLOW-3D HYDRO)**
  - Compare to 2D results and confirm 2D model assumptions were appropriate
- **Physical Model Testing (Alden Laboratories)**
  - Test designed riprap stability at 65% design phase
- **Unsteady Sediment Transport Modeling (2D HEC-RAS)**
  - Estimate scour in unarmored areas adjacent to end treatment to inform design and maintenance





# Hydraulic Design Criteria and USACE Guidance



- **Modeling Criteria**

- Utilize pre-calibrated 2D HEC-RAS model and terrain supplied by USACE
- Utilize manning's n-values of 0.039 and 0.041 for R2200/R7400
- Utilize minimum HW/TW differentials
  - **White to Arkansas Rivers 8-ft (2011 Event)** ← **Governing Storm Event**
  - Arkansas to White Rivers 6-ft (1990 Event)

**Predominant Flow Condition  
(Focus of Presentation)**

- **Riprap Design**

- Must be used in areas where velocities > 1.5 fps
- Minimum gradation at any location is R2200
- Minimum gradation where velocities > 10.0 fps is R7400
- Minimum thickness of  $2.0 * D_{50}$  or  $1.5 * D_{100}$
- Utilize standard USACE gradations - R2200/R7400
- Utilize Isbash equation (high turbulence assumption) with 2D model results for sizing



Hydraulic Analyses

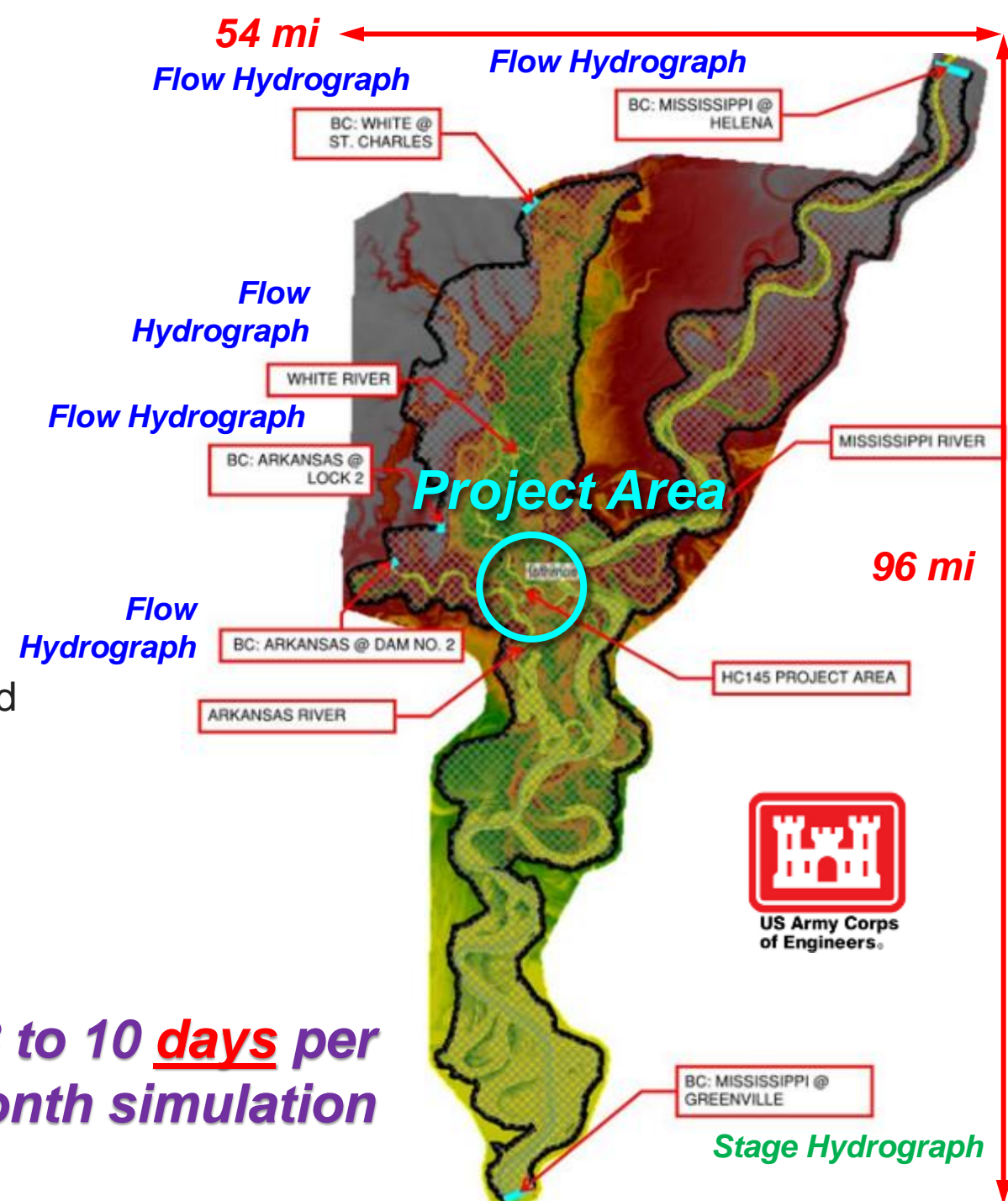
# 2D HEC-RAS Modeling



# Large Domain Model

- Base model and terrain model covers 5,200 mi<sup>2</sup>
- **Models used to confirm HW/TW differentials from 1990 and 2011 historic events**
  - Base model
    - 1,500-ft x 1,500-ft Grid Cells (~25,000 Cells)
  - w/Project model
    - Includes 6.75-ft to 75-ft resolution around project area (~ 37,000 Cells)
- Used combination of flow and stage hydrographs on White, Arkansas and Mississippi Rivers

*\* Run times at 8 to 10 days per multi-month simulation*



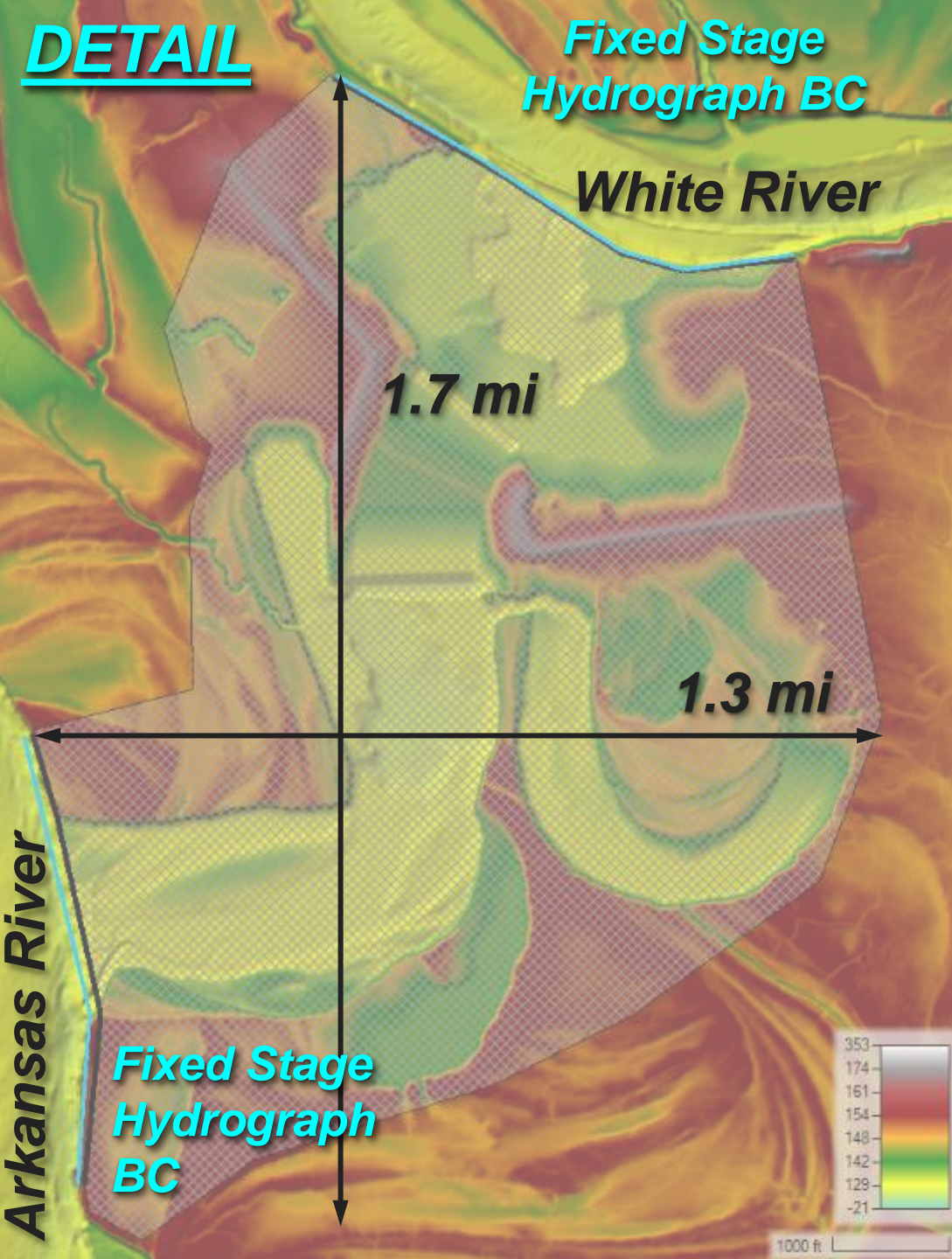
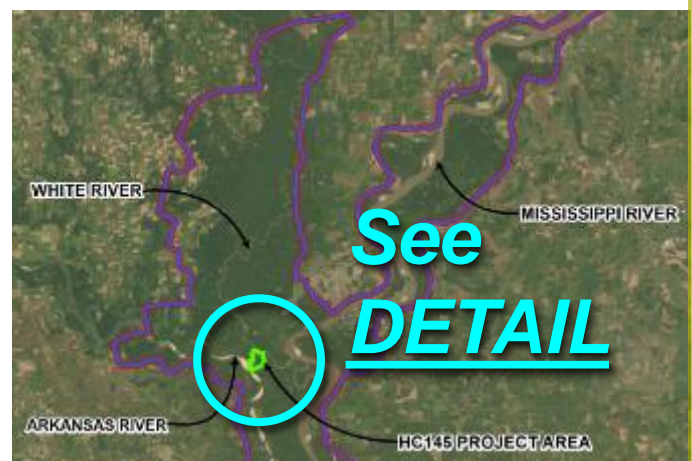




# Small Domain Model

- Small subset of large domain model covering project area (~2 mi<sup>2</sup> down from ~5,200 mi<sup>2</sup>)
- **Models used to rapidly test weir and grading alternatives**
- HW/TW levels set to constant stage hydrographs covering target HW/TW differentials to expedite model runtimes
- **Final w/project alternative inserted and validated within large domain model**

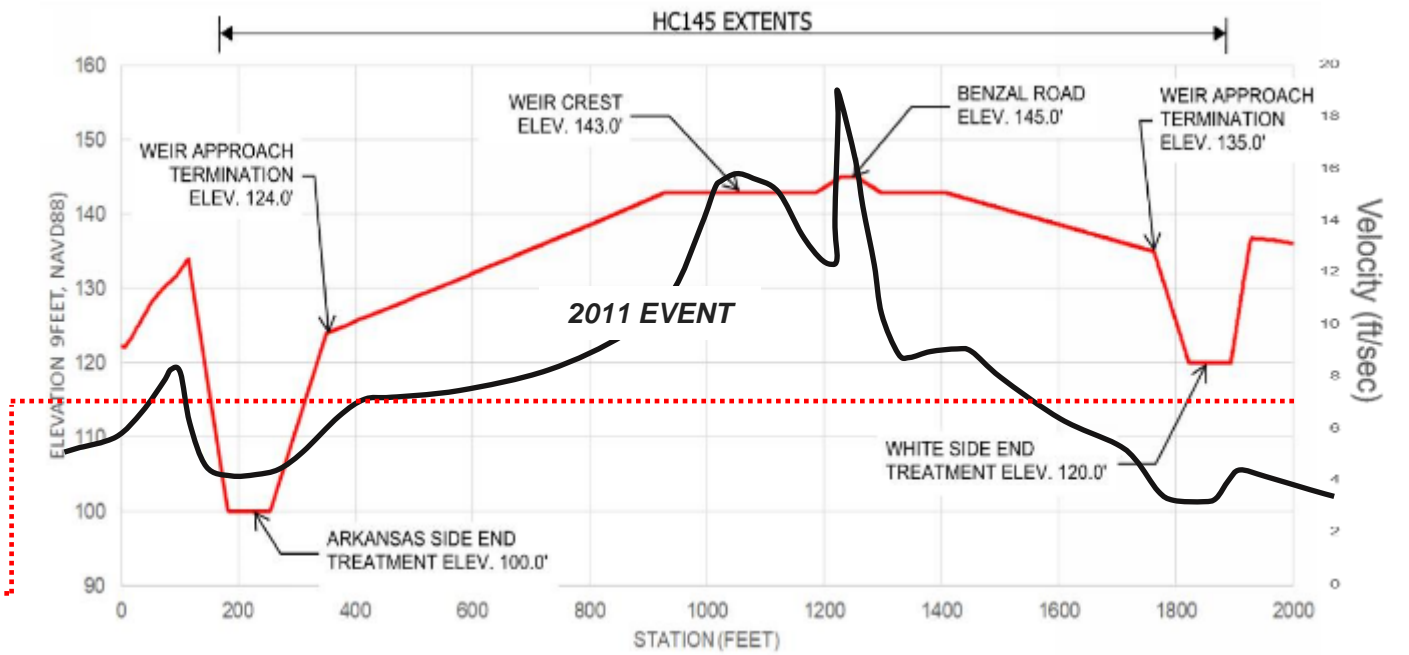
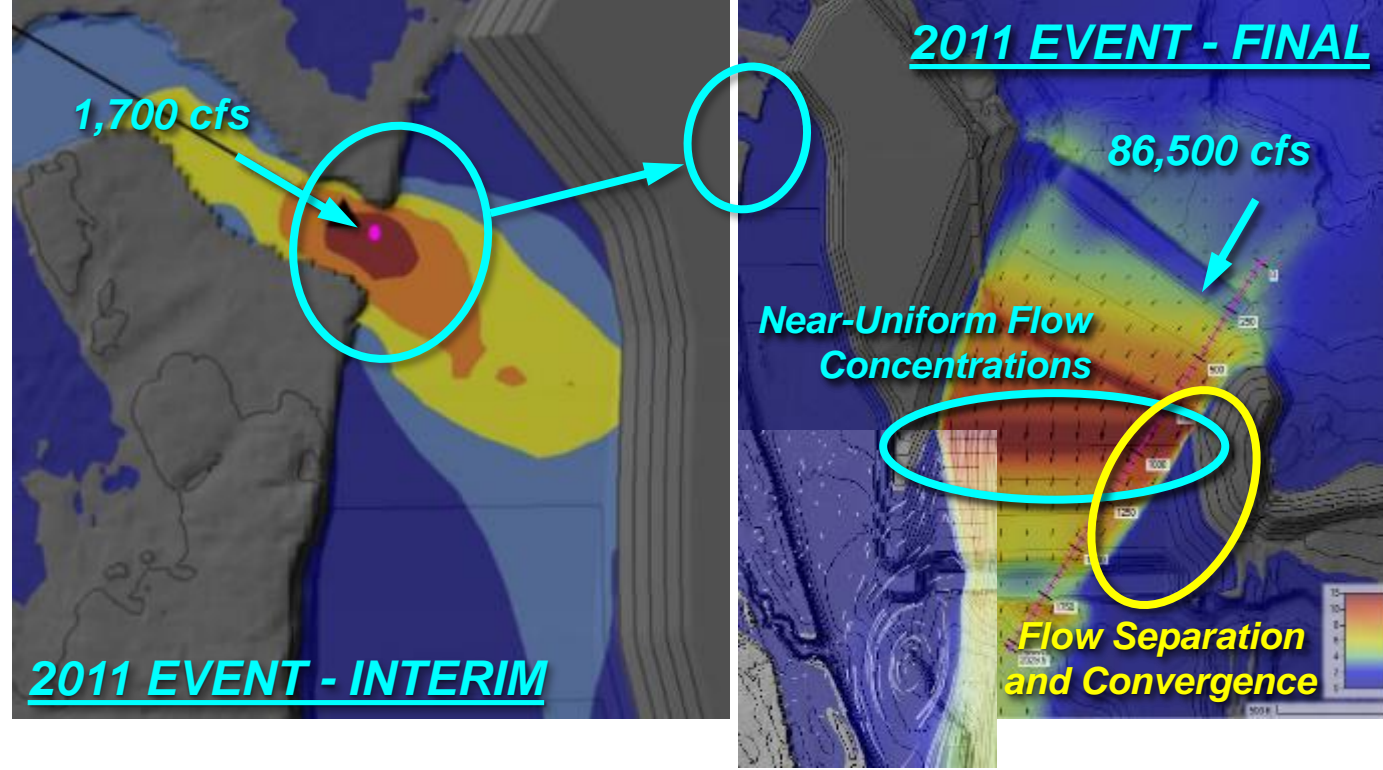
*\* Run times at 2 to 4 hours per steady-state simulation*





# Small Domain Model Results

- **Maximum depth-averaged velocities met USACE design criteria**
  - Velocities ranged from 7 to 20 ft/s within project area
- **Near-uniform flow concentrations achieved near weir crest**
- **Flow Separation and convergence observed along weir approach slope**



**Allowable Velocity Threshold at Termination of Approach Slope**



Hydraulic Analyses

CFD Modeling

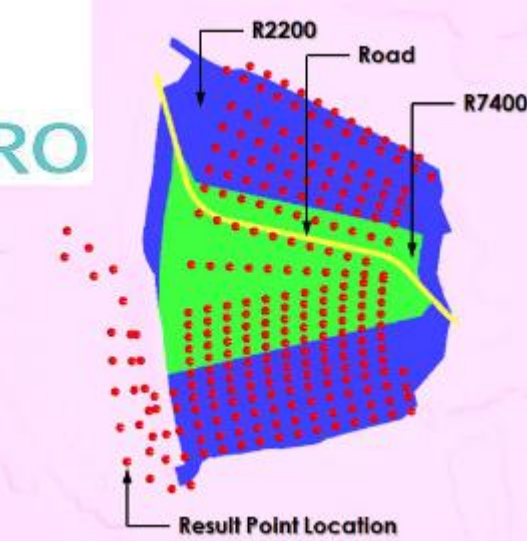
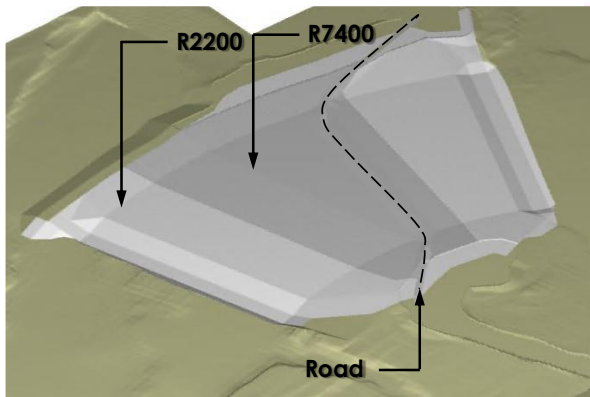


*\* Run times at 3 to 5 days per steady-state simulation*

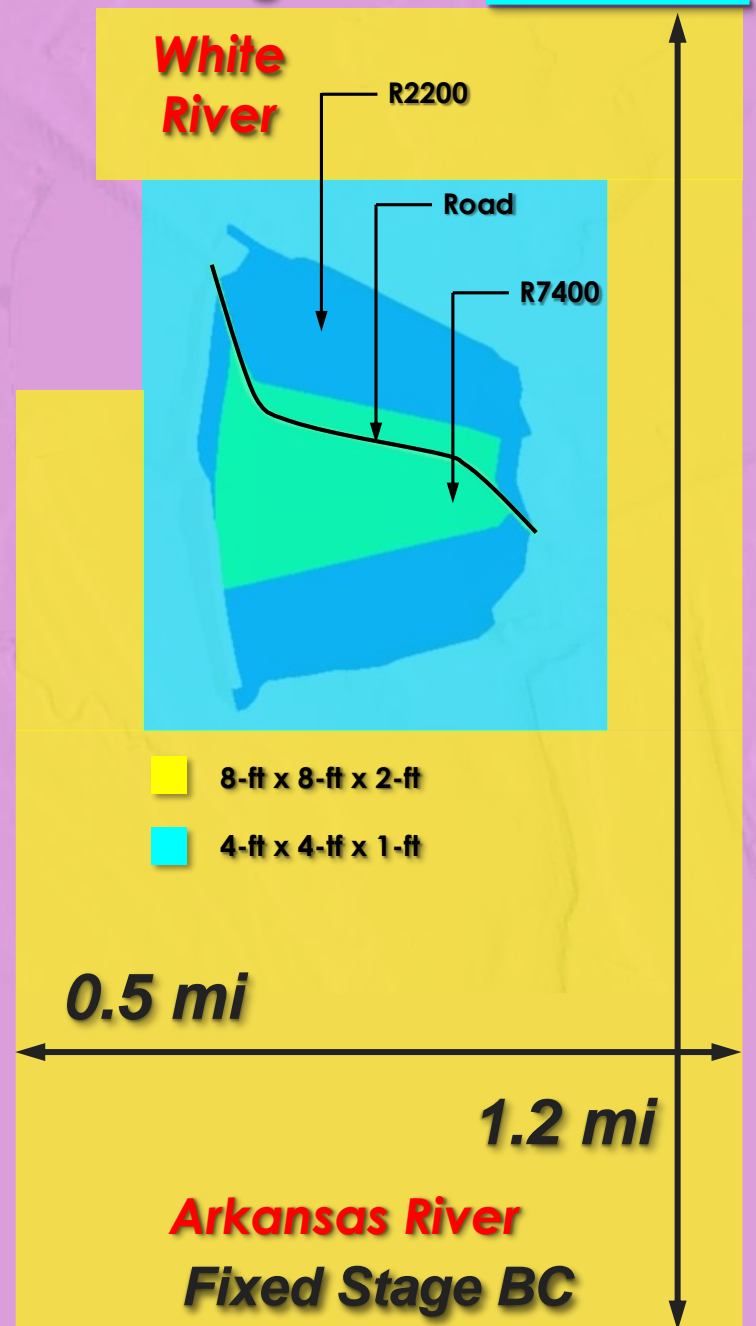
# CFD Model

- Subset of small domain 2D model (~0.6 mi<sup>2</sup> down from ~2.0 mi<sup>2</sup>)
- HW/TW differentials and boundary conditions matched small domain 2D HEC-RAS modeling approach
- **Models Used To:**
  - **Compare/Confirm 2D model results and assumptions were appropriate using a gridded approach**
  - Provide full 3D velocity field data for use/consideration in physical model and riprap design

## FLOW-3D<sup>®</sup> HYDRO



**Fixed Stage BC** **DETAIL**

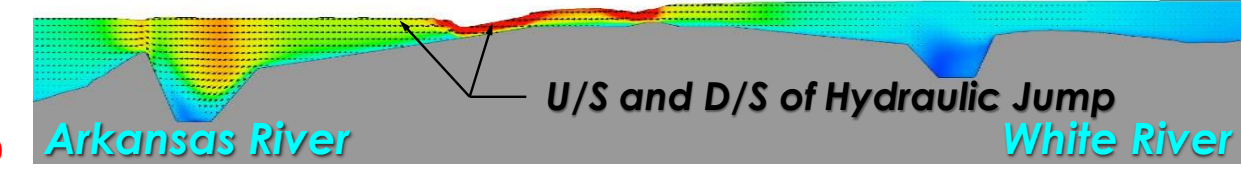
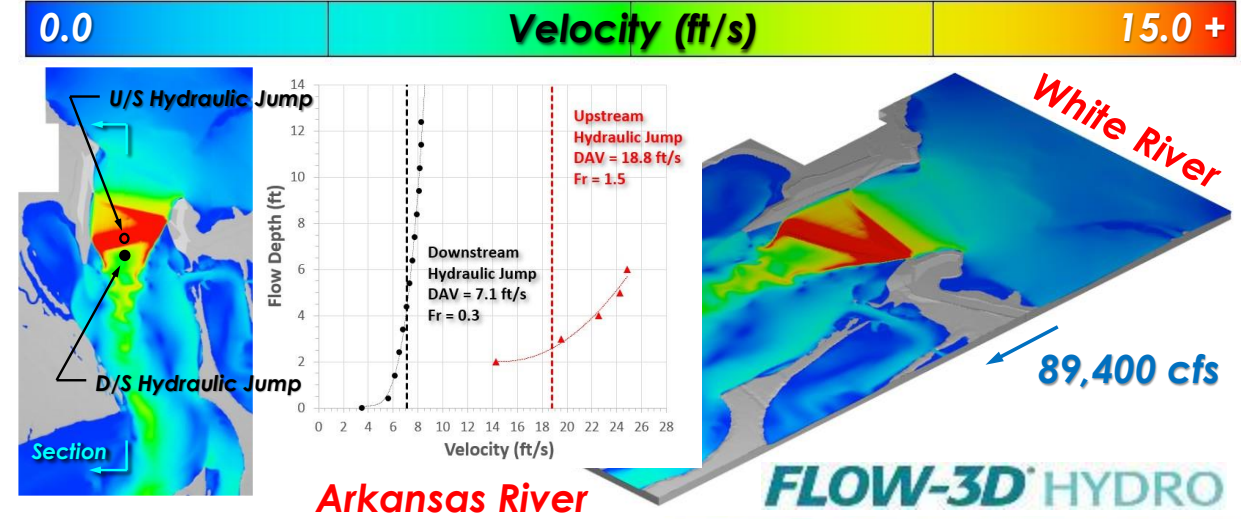
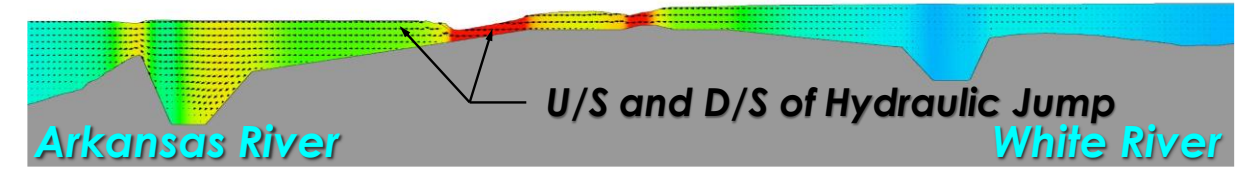
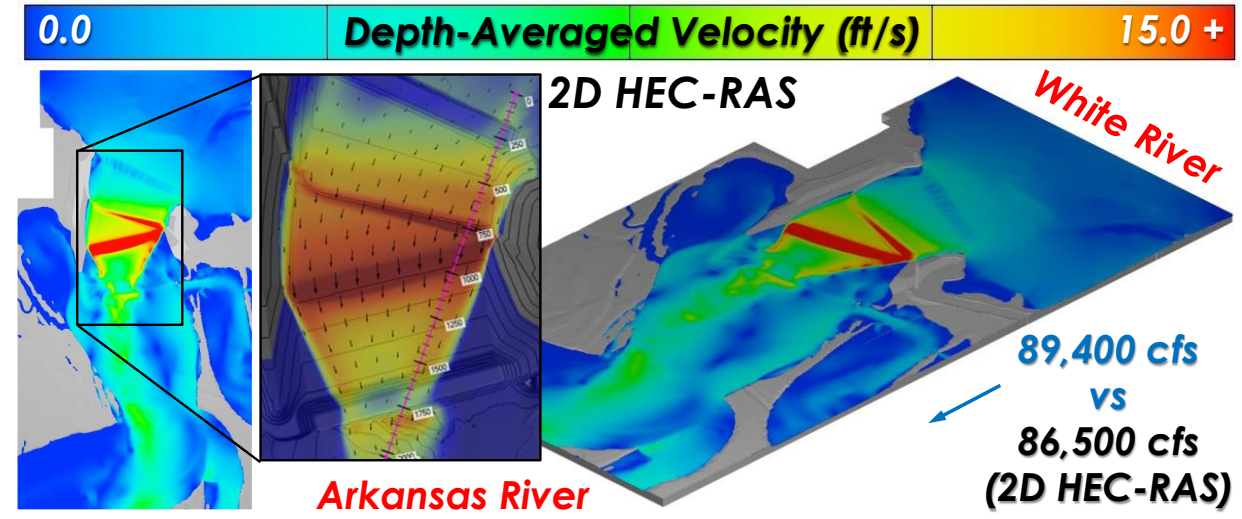
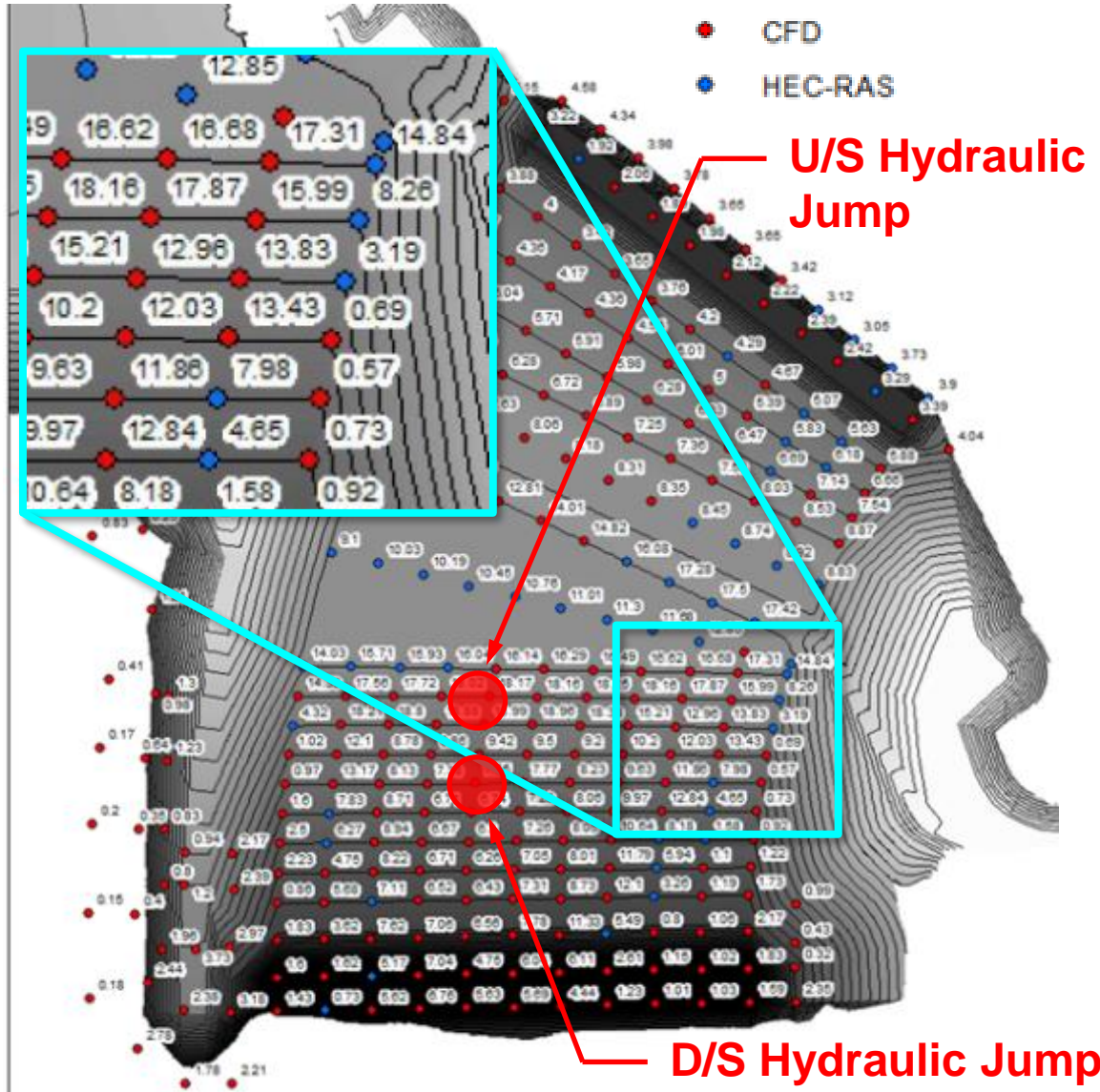






# CFD Model Results

THREE RIVERS, HC145 - 2D HEC-RAS MODEL



Hydraulic Analyses

# Physical Model Testing





# Physical Model Testing

- 1:20 scale model
- “Unit” width model
  - 5-ft model scale represents 100-ft prototype scale
- **Used to evaluate riprap movement and stability**
- Physical model testing prepared by Alden Laboratory (Holden, MA)

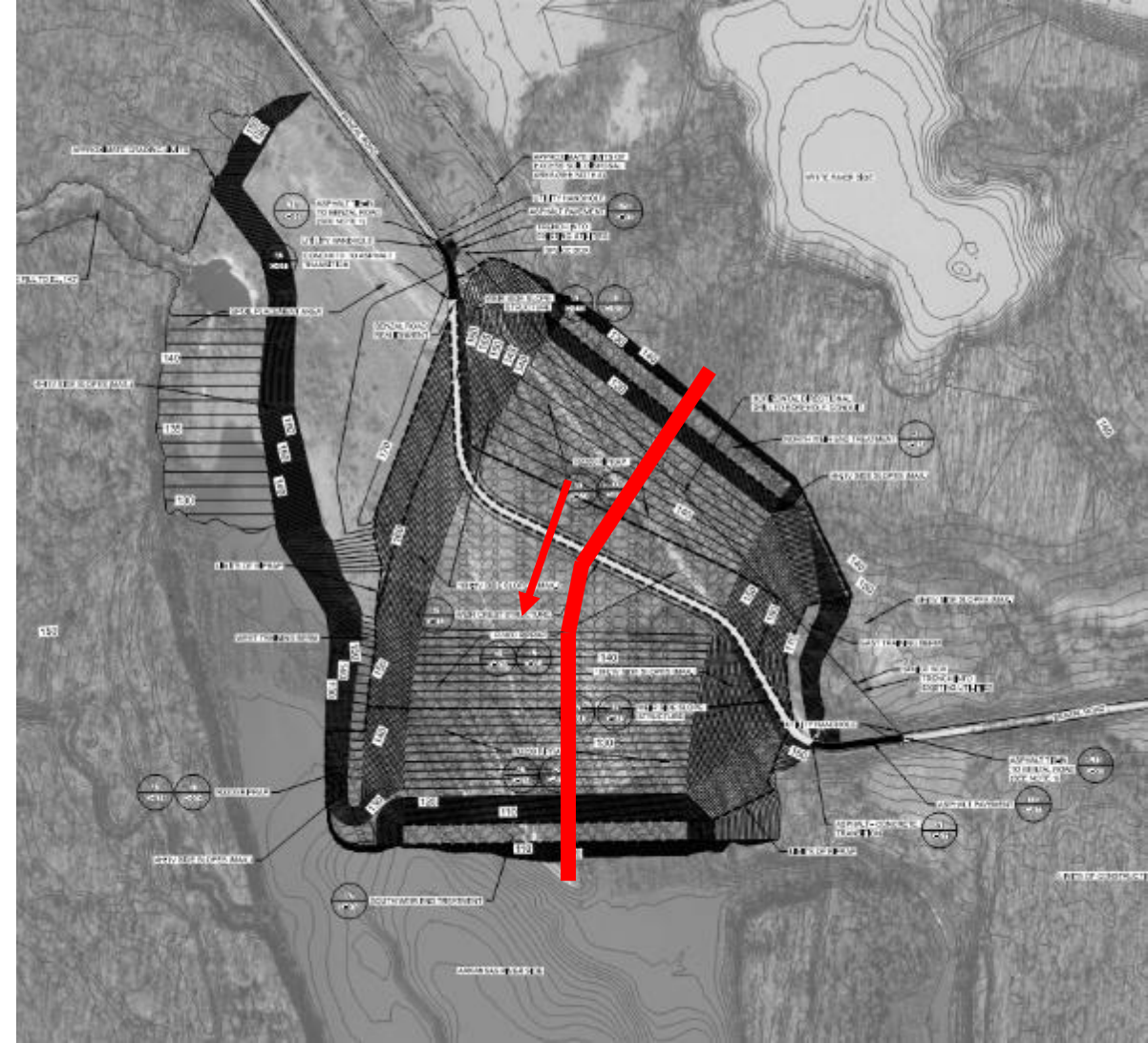
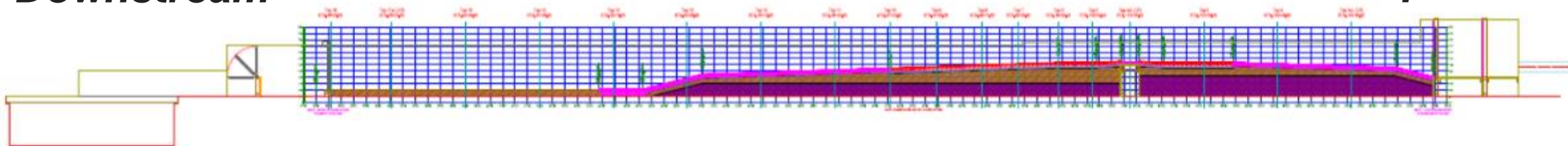
**ALDEN**  
Solving flow problems since 1894

**Downstream**

**Flow**  
←

**Weir Crest**

**Upstream**





# Physical Model

- Water-tight wood frame
- Recirculating pump flow loop







# Physical Model

- Stone painted to support visual observations of movement

**ALDEN**  
Solving flow problems since 1894











# Physical Model

- **Test Plan:**
  - Design Scenarios
  - Low Probability Events
  - Flow Convergence
  - Long Duration Event

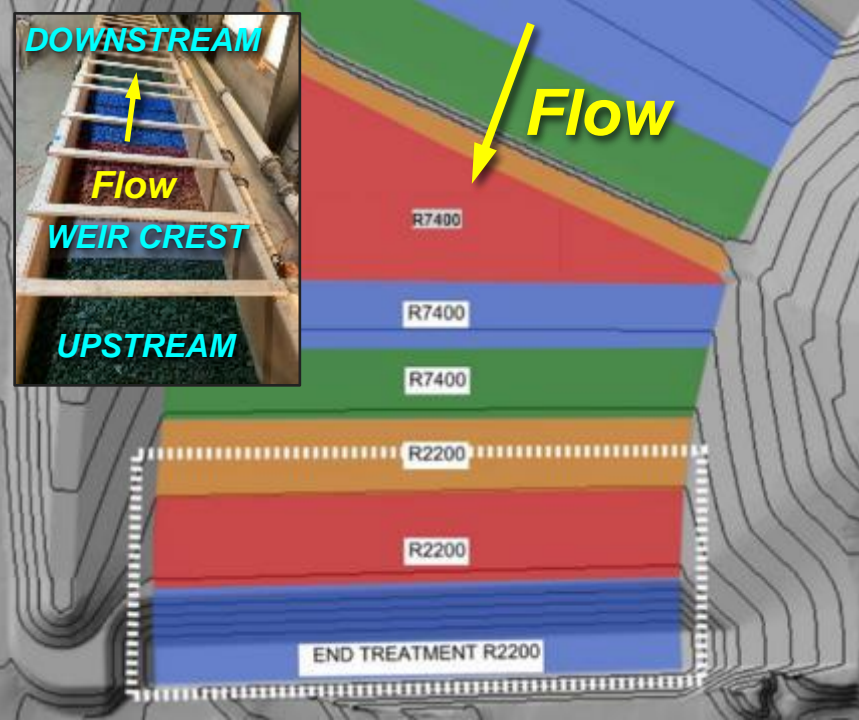


Table 1. Physical Model Test Plan

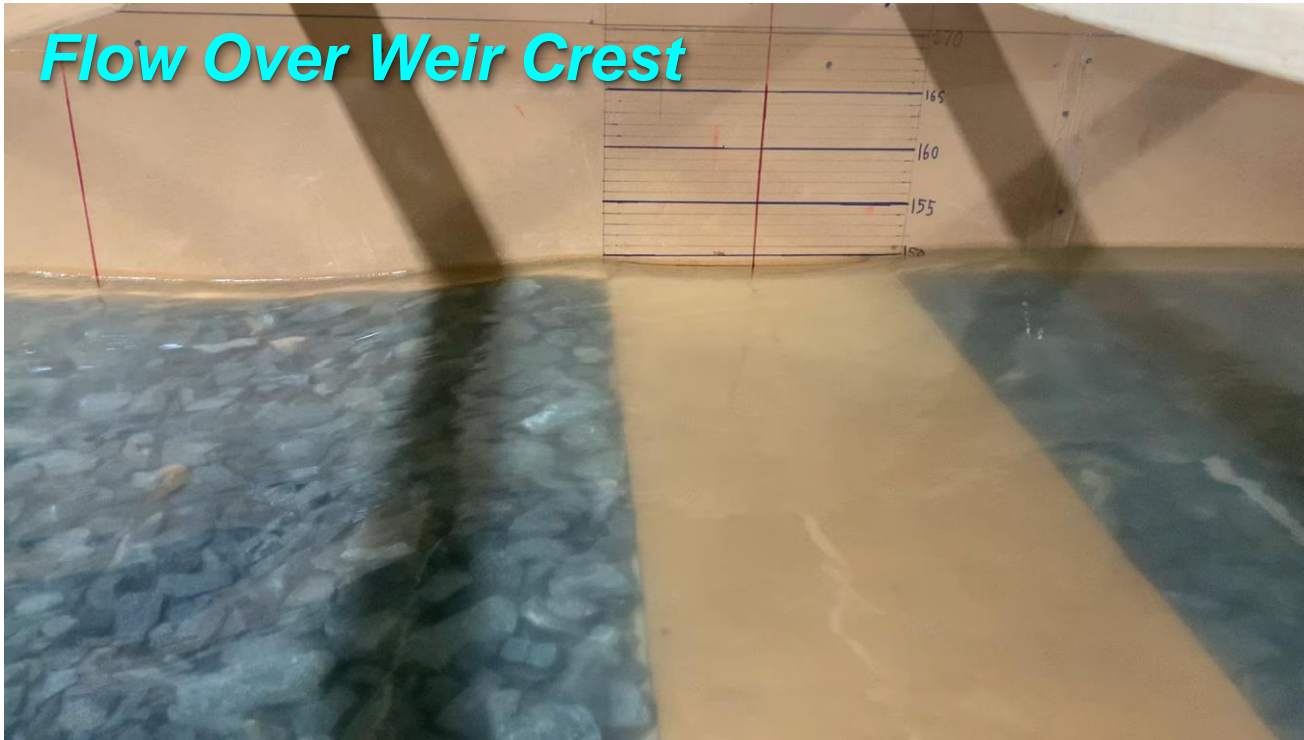
Test Number	Headwater (WSE, ft)	Tailwater (WSE, ft)	Target Unit Discharge (Q, cfs/ft)	Test Case No. and Description
1	146	138	--	2 – Event that just overtops the HC145 crest
2	147	141	--	1 – 1990 Design HW/TW Differentials used for design
3	150	142	--	2 – Event producing 8-ft differential with shallow weir flow
4	155	147	--	1 – 2011 Design HW/TW Differentials used for design
5	160	155	--	3 – Low probability event based on Copula
6	161.3 <sup>1</sup>	160	--	3 – Low probability event
7	168.0 <sup>1</sup>	168	--	3 – Low probability event
8	-	165	145	4 – Flow convergence (End Treatment & R2200, Stations 92+54 to 95+00)
9	-	155	135	4 – Flow convergence (End Treatment & R2200, Stations 92+54 to 96+00)
10	-	155	150	4 – Flow convergence (End Treatment & R2200, Stations 92+54 to 95+20)
11	-	165	160	4 – Flow convergence (End Treatment, Stations 92+54 to 94+24)
12	-	147	130	4 – Flow convergence (End Treatment, R2200, Stations 92+54 to 96+50)
13	-	147	155	4 – Flow convergence (End Treatment, R2200, Stations 92+54 to 95+00)
14	-	147	130	5 – Long Duration with three, 8-hour runs. (End Treatment, R2200, & R7400, Stations 92+54 to 96+50) Same conditions as in Test 12

1. Indicates actual headwater WSE that was achieved during testing due to constraints of pumping capacity



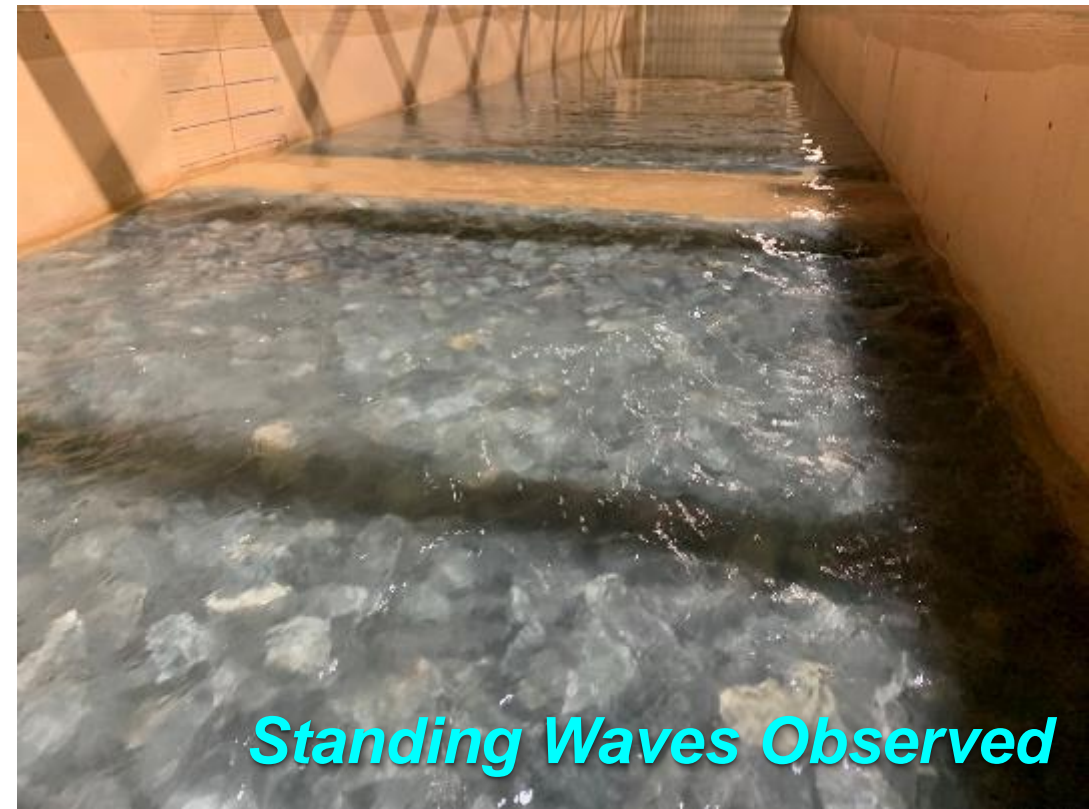


# Physical Model Results



**2011 EVENT - FINAL**

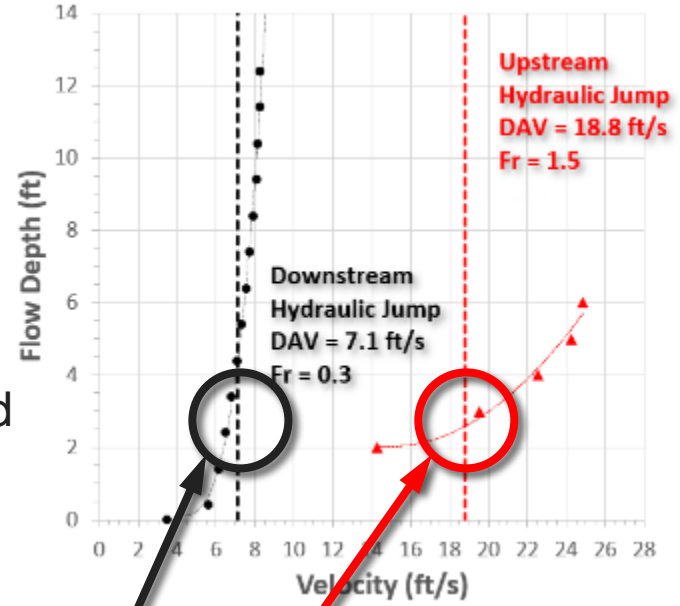
**ALDEN**  
Solving flow problems since 1894





# Physical Model Results

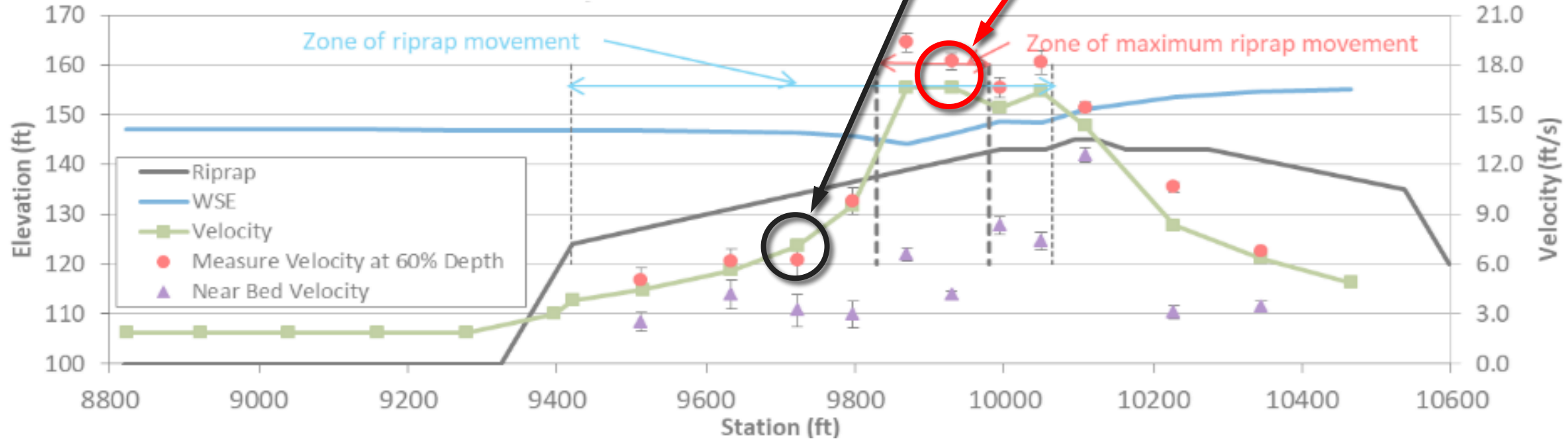
- **Hydraulic Performance**
  - Velocity, hydraulic jump location(s) showed good correlation with CFD results
- **Riprap Movement**
  - Some movement of individual stones anticipated



**CFD RESULTS**

## 2011 EVENT FINAL

**ALDEN**  
Solving flow problems since 1894







# Physical Model Results

- **Challenge: Results Interpretation**
  - Some riprap will move – what is acceptable?
  - Table summarizes percent of stones moved in each region



Figure B- 56: Camera 4, Post [Test 13](#).



Figure B- 70: Camera 5, Post [Test 13](#).

Riprap Class	Location	Station Range	# Stones Moved	% Area of Region	Located Within Test Focus Area?
R7400	Road to Crest Transition (Orange)	100+55 to 100+95	4	0.46%	No
R7400	Weir Crest (Red)	99+94 to 100+55	3	0.22%	No
R7400	Weir Approach Slope (Blue)	98+71 to 99+94	20	0.67%	No
R7400	Weir Approach Slope (Green)	97+26 to 98+71	57	1.92%	No
R2200	Weir Approach Slope (Orange)	95+80 to 97+23	13	0.19%	No
R2200	Weir Approach Slope (Red)	94+24 to 95+80	8	0.12%	Yes





# Physical Model Results

- **Conclusions:**

- Riprap stability is a function of stone size, layer thickness and interlocking
- Rolling/flipping of individual stones observed during testing, but stones settled back into riprap layer and did not remobilize
  - These stones were likely sticking up into flow and not locked in upon initial placement
- No concentrated movement, no movement of more than isolated stones observed
- Riprap configuration deemed acceptable based on model results



Hydraulic Analyses

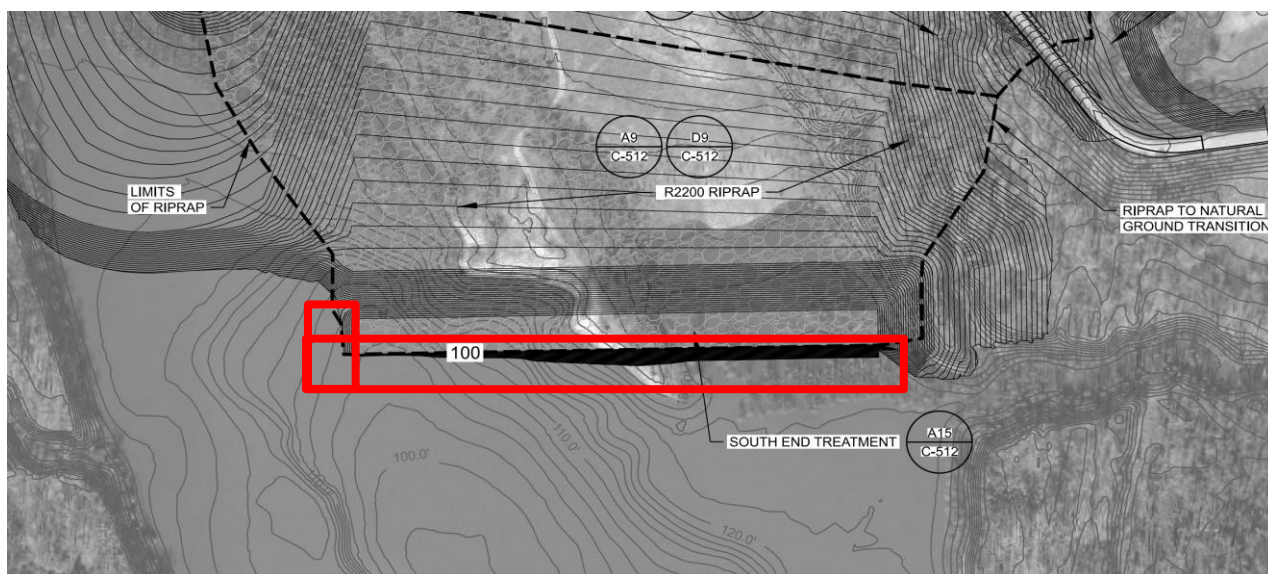
# Sediment Transport Modeling





# Purpose & Approach of Sediment Modeling

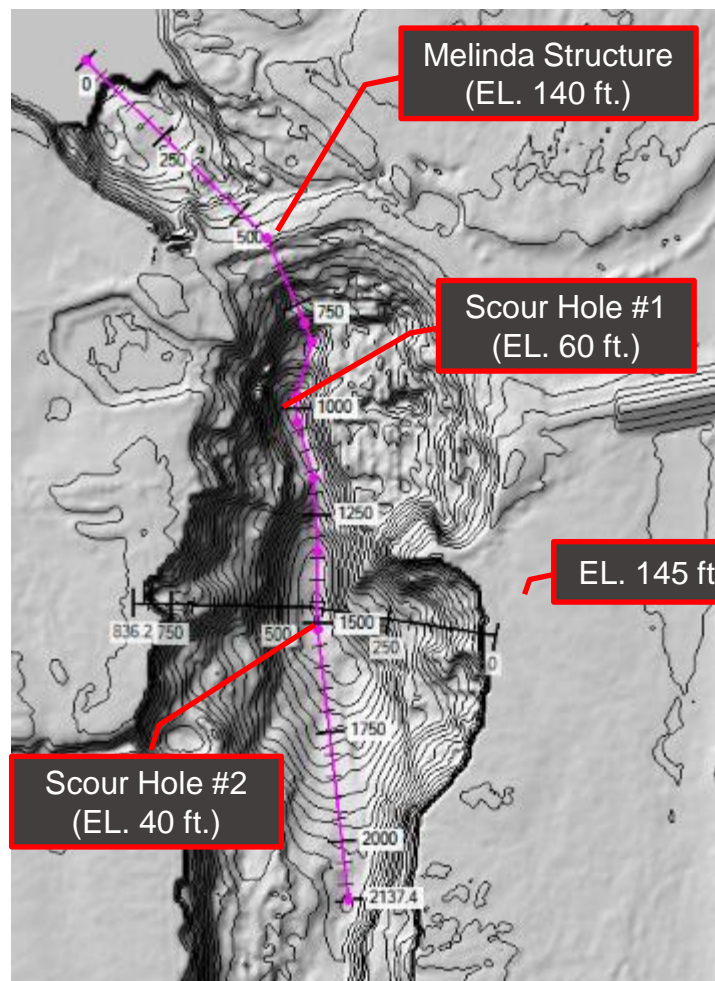
- **Purpose**
- Evaluate potential scour formation
  - Southern end treatment
  - Sustained weir topping event (2011)
- Utilize scour results for design and O&M plan
  - Inform design measures
  - Estimate potential maintenance needs
- **Approach**
- Utilize available project data
  - 2D HEC-RAS and 3D CFD models
  - Geotechnical investigation
- Implement HEC-RAS 2D sediment transport modeling capabilities
- Perform sensitivity analysis of sediment transport modeling parameters
  - Inform selection of “best estimate” parameter set(s) to use in 2011 event simulations
- Utilize scour results from 2011 event simulation to inform design and O&M plan





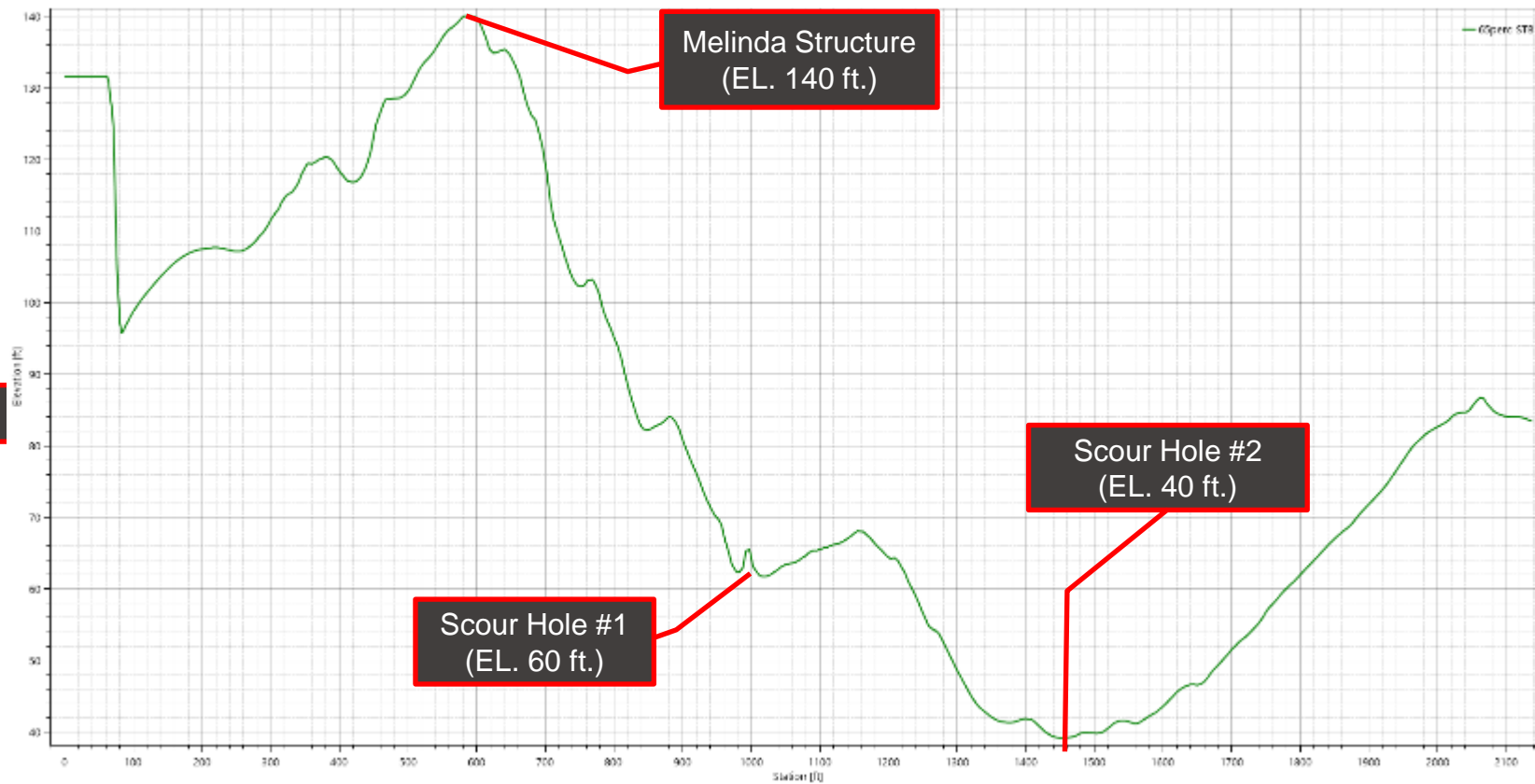
# Purpose & Approach of Sediment Modeling

- Why are we concerned about scour?



Melinda Structure

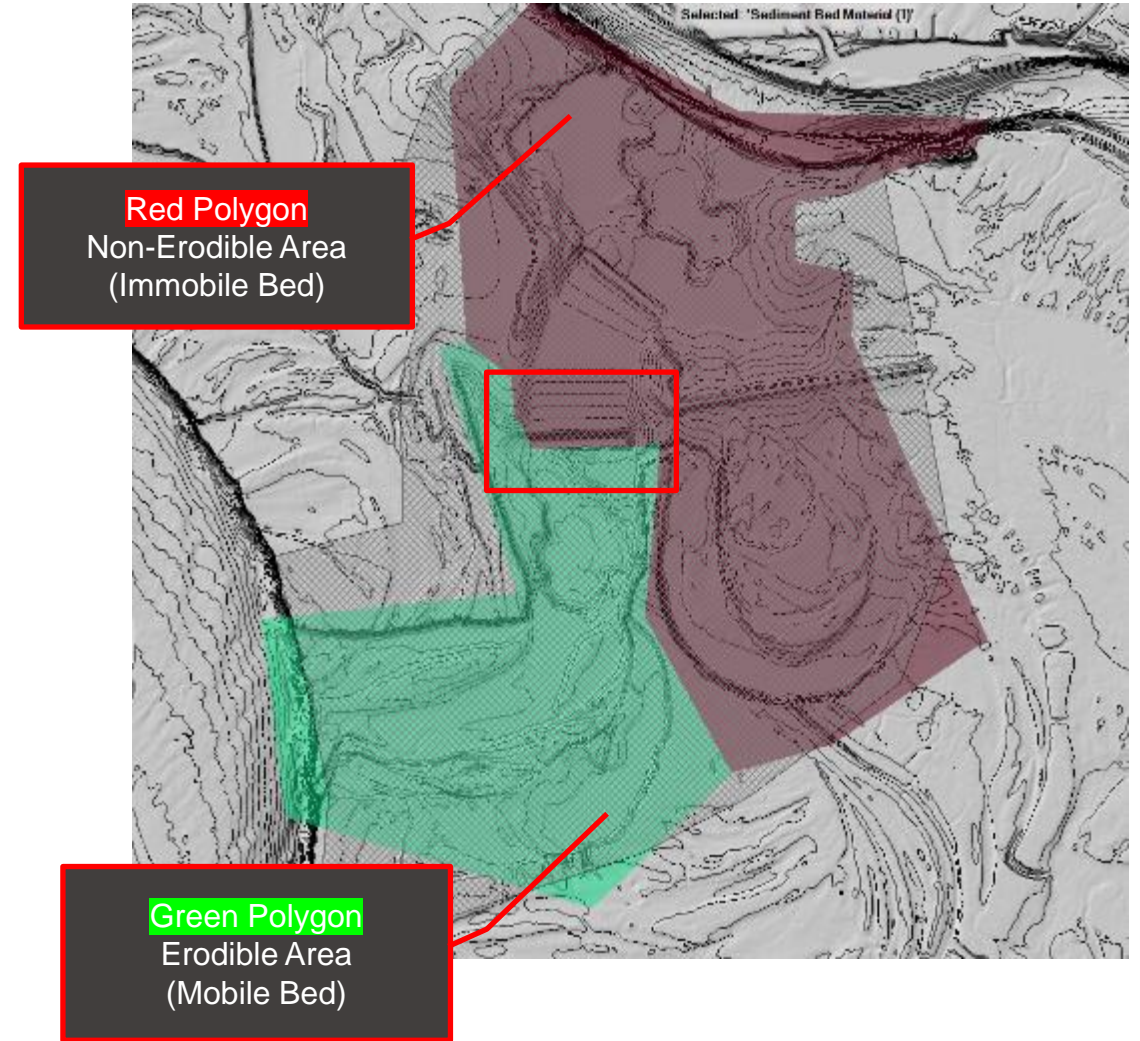
HC145 Structure





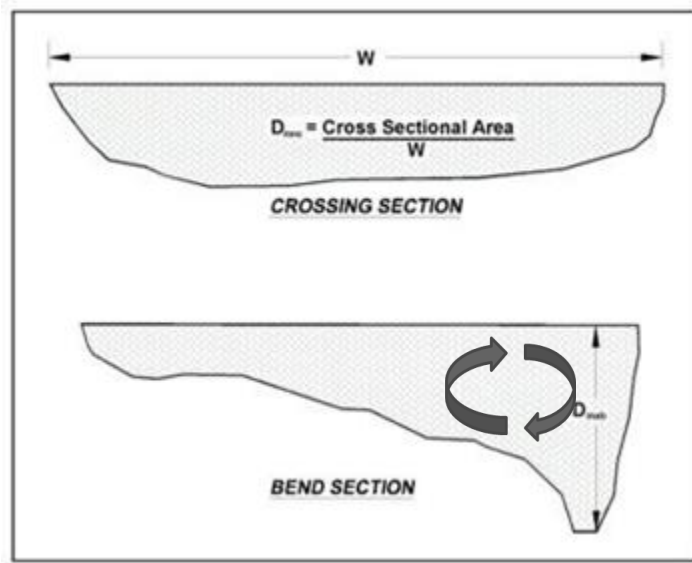
# Model Setup, Data Inputs and Assumptions

- **2D Sediment Bed Material Map Layer**
  - RAS Mapper
  - Erodeable area limits defined
- **Sediment Data File**
  - Sediment transport computation settings
  - Defined bed gradation(s)
  - Associated to 2D mapped layer surfaces
  - Utilized non-cohesive soil gradations & properties only
  - Predominant soil types are non-cohesive
    - Poorly graded sand (SP) & silty sand (SP-SM)
  - Cohesive soils in project area are sparse, not included
- **Single Bed Gradation Applied**
  - Assessed lab data from predominant soil samples
  - Sensitivity analysis of fine to coarse gradations
  - Conservative gradation selected for use in 2011 event run

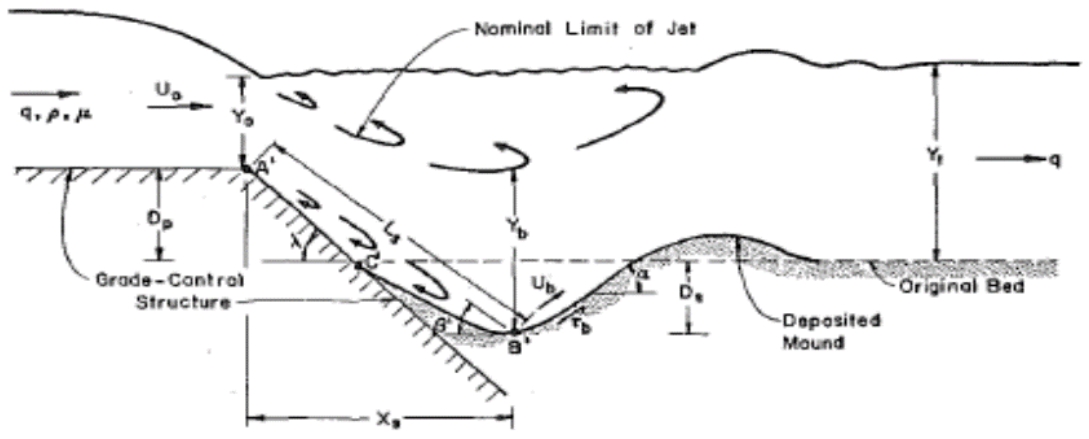


# Sediment Modeling – Limitations & Uncertainties

- Vertical variation in water column is not represented
- Vertical circulations not represented
- Local scour due to complex flow patterns may not be well represented
- Pool scour in pool-riffle complexes is often under predicted
- Bank erosion prediction is still in research stage



<p><b><u>Known-Knowns</u></b></p> <ul style="list-style-type: none"> <li>• Your experience</li> <li>• Measured input data</li> </ul>	<p><b><u>Known-Unknowns</u></b></p> <ul style="list-style-type: none"> <li>• <b>Model Uncertainty</b></li> <li>• Future hydrologic conditions</li> </ul>
<p><b><u>Unknown-Knowns</u></b></p> <ul style="list-style-type: none"> <li>• Lack of experience, knowledge, or training</li> <li>• Lack of data</li> </ul>	<p><b><u>Unknown-Unknowns</u></b></p> <ul style="list-style-type: none"> <li>• Unaccounted processes</li> <li>• Unidentified factors</li> </ul>



*modified from Borman and Julien [1991].*

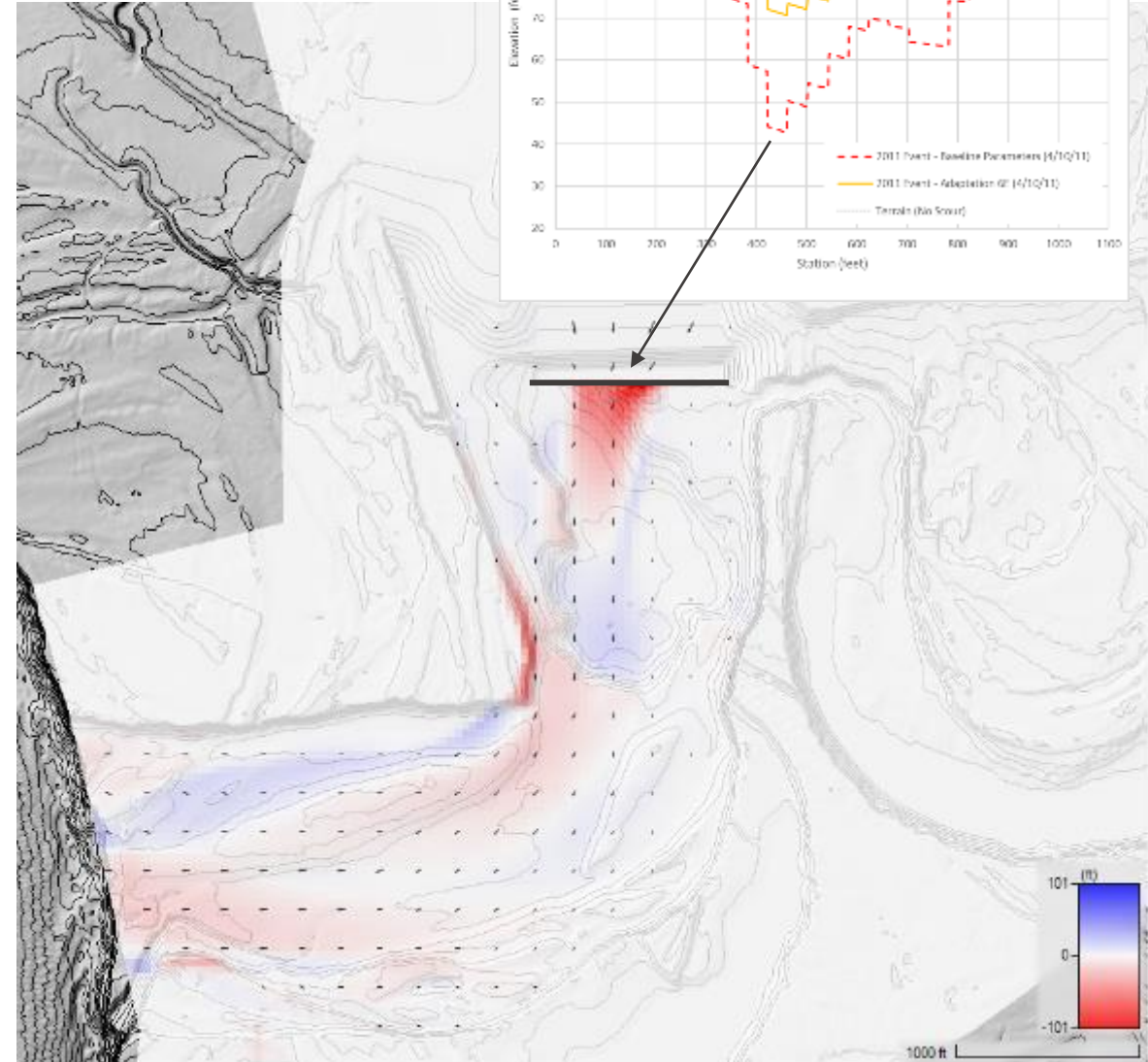




# 2011 Event Scour Results Summary

- Results have limitations, but can be used to inform potential outcomes
- Results show scour concentrating near the center of south end treatment
- Deepest scour located along face of end treatment between EL. 40 to 70 feet
- Scour elevations are comparable to historic scour at the Melinda Structure
- **Conclusion:**
  - **Scour in un-armored areas downstream of weir is likely to occur**

**2011 EVENT FINAL**

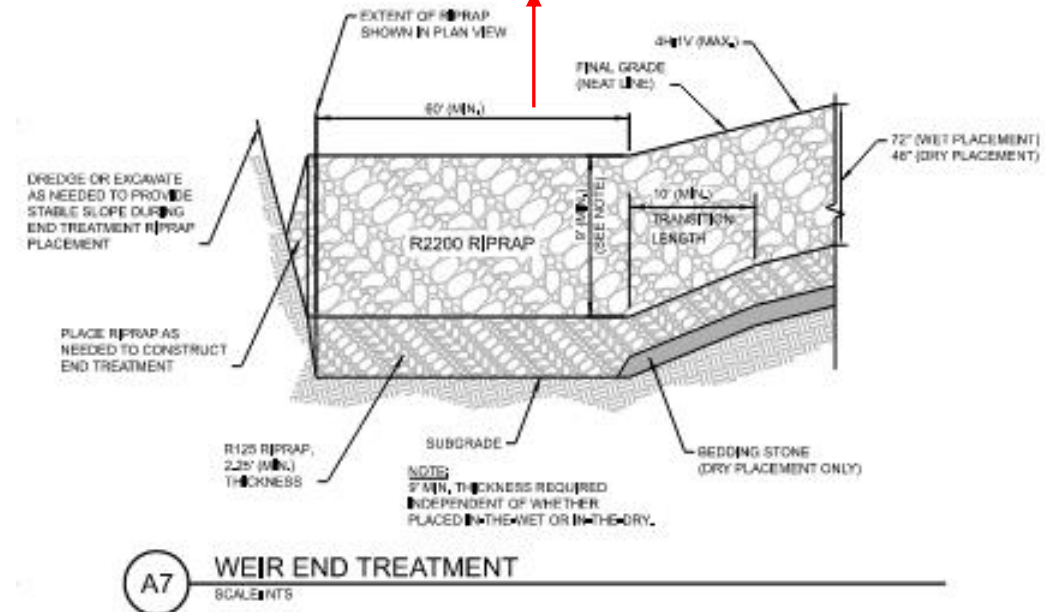
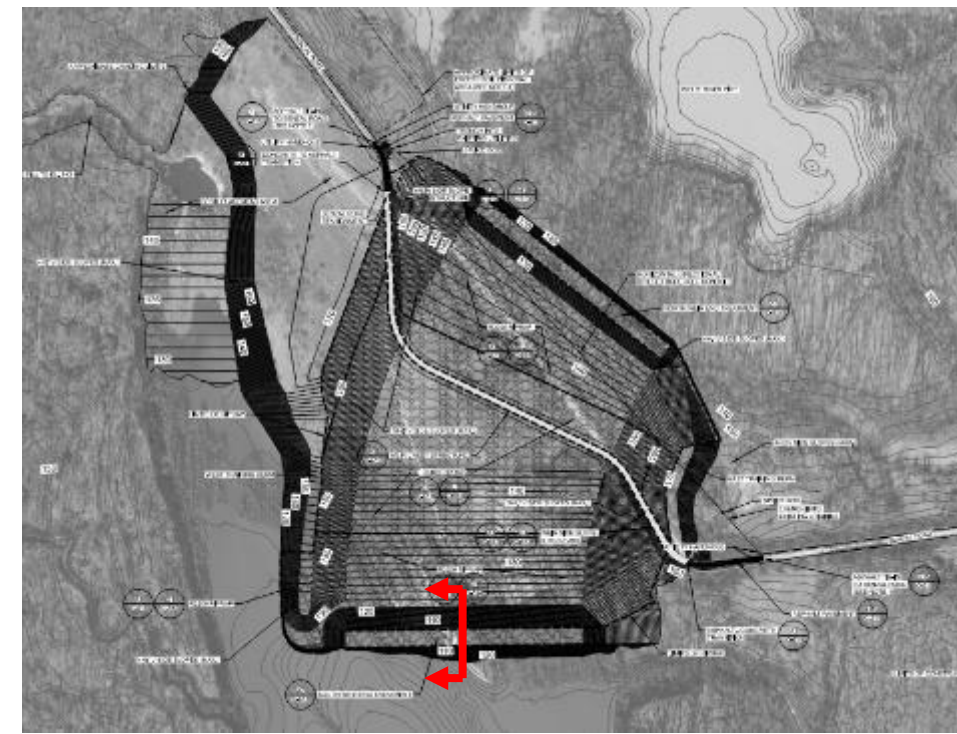
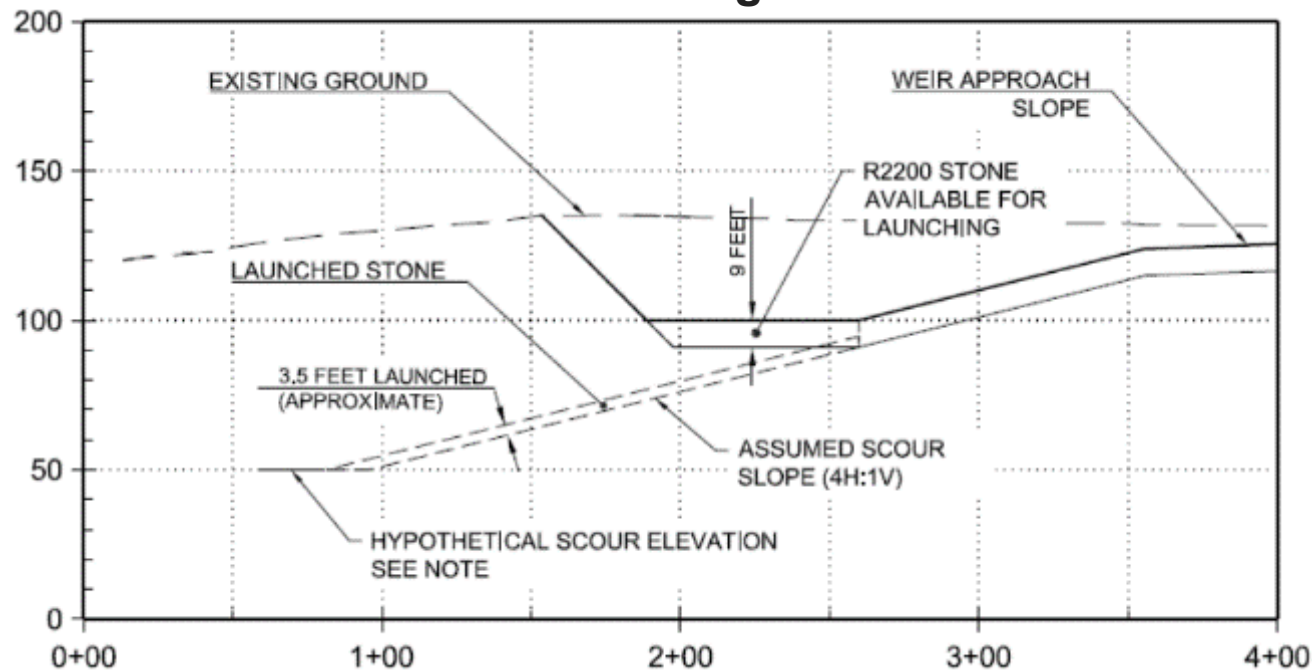




# Design Application

- Launching riprap toe included in design
- O&M to include periodic surveys and addition of supplemental riprap as necessary

## Potential “Launched” Configuration







# Takeaways

- Establish modeling framework at beginning of project is important
- Define clear goals for and acknowledge limitations of each model being considered
- Pay close attention to limitations and uncertainties when interpreting model results







***Stantec Consulting Services Inc.***

***Matthew Hoy, PE***

***Justin Bartels, PE, CFM***

**Questions?**